

An Optically Powered Radio over Fiber Remote Unit using Wavelength Division Multiplexing

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Abstract— Power over fiber and radio over fiber transmission have been combined in a single optical fiber using wavelength division multiplexing for the first time. It is shown that there is no impairment to the radio over fiber transmission performance from the power transmission link. There is however a power penalty caused by the insertion losses of the multiplexer and demultiplexer and potentially a further insertion loss depending on the type of transmission fiber used.

I. INTRODUCTION

The combination of power over fiber and radio over fiber to achieve optically-powered remote radio units has been proposed and experimentally demonstrated previously [1]. There it was concluded that optical powering was a feasible technique for many radio over fiber applications, especially in-building distributed antenna systems in situations where providing remote electrical power outlets is impractical, expensive or hazardous. Examples of where this would be useful include high voltage environments in electricity substations and in petrochemical plants where sparking may cause explosions. Radio over fiber is widely acknowledged as an excellent technique for simplifying the remote units required at antenna sites for wireless communications systems [2] and the use of power over fiber takes this simplification process a stage further by removing the need for electrical outlets at the antenna sites.

Separate optical fibers were used for optical power transmission and for radio signal transmission in [1], so that each fiber type could be optimized for its intended use. For power transmission, the fiber had a core diameter of 62.5 μm (the largest core diameter in common use for in-building data networks), whereas for radio signal transmission the fiber had a core diameter of 50 μm (high bandwidth fiber, optimized for short wavelength optical sources). In this paper we investigate the use of wavelength division multiplexing to achieve optical power transmission and radio signal transmission over a single fiber.

II. COMPONENT SELECTION

A. Power Laser and Photovoltaic Converter

High power semiconductor lasers are available commercially with a variety of wavelengths and powers. The lasers with the highest output powers are multiple transverse mode devices with wide active layer widths. The available optical power scales with active layer width: for example, the JDSU 2300 series of high power lasers at 810 nm wavelength provide approximately 1 W of power per 100 μm of active layer width [3]. Some fiber-coupled lasers provide even higher levels of power: for example, the JDSU 2486-L3 series lasers provide up to 2 W into a 60 μm fiber at 830 nm [4] and the JDSU 2495-L3 series lasers provide up to 4 W at 808 nm into a 105 μm fiber [5]. The work in [1] used a JDSU power laser with a fiber-coupled output of up to 2 W into 62.5 μm fiber, chosen as a compromise between the need for high levels of optical power and compatibility with standard fiber types used for in-building data networks. This work uses the same laser for the same reasons. The wavelength of this laser is 834 nm, which was chosen to be compatible with the PPC-4E from JDSU, the only fiber-coupled photovoltaic converter that is commercially available to the authors' knowledge. The PPC-4E is also compatible with 62.5 μm core diameter fiber.

B. Transmission Fiber

The transmission fiber should be multimode to accommodate the high levels of optical power provided by the high power laser. Multimode fiber dominates the in-building data network installed base [6]; it is clearly available and useful for deploying systems such as that described here for reasons of convenience and cost. This installed base multimode fiber has a core diameter of either 50 μm or 62.5 μm , with roughly equal predominance worldwide. The

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62.5 μm core diameter fiber would be the obvious choice to use in this work since it is compatible with the choice of high power laser. However, there are potential deployment scenarios where, for example, only 50 μm fiber might be available for use. Furthermore, it is instructive to analyze the power penalty involved when using a transition from 62.5 μm fiber to 50 μm fiber, especially when a multimode laser is used as the optical power source. This transition penalty can vary from 0 dB to around 4 dB depending on the type of optical source [7]. From a signal transmission perspective, the over-filled launch bandwidth of 62.5 μm fiber is less than that of 50 μm fiber, but the actual bandwidth of each fiber type is very similar when using laser sources. It has been shown previously that multimode fiber with low over-filled launch bandwidth can have a good response beyond this bandwidth if a restricted number of modes are excited in the fiber during launch [8,9]. Therefore, a transmission fiber with a core diameter of 50 μm was chosen for this work, allowing us to analyze the transition penalty problem.

C. Signal Laser and Photodiode

Most radio over fiber systems operate at a wavelength of 1310 nm using either Fabry-Perot (FP) or distributed feedback (DFB) lasers and InGaAs pin photodiodes. This wavelength is chosen because low cost components with good analog performance are available from a number of suppliers. The work in [9] used both FP and DFB lasers with a wavelength of 1310 nm and showed that good radio over fiber performance was achievable using fiber with a 50 μm core diameter. The choice of laser used for this work was a 1310 nm FP device and the photodiode was a conventional InGaAs pin device in a receptacle package that was compatible with multimode fiber.

D. WDM multiplexer and demultiplexer

The wavelengths of 834 nm and 1310 nm and fiber core diameter of 50 μm dictate the main specifications of the wavelength division multiplexer used. Additional important requirements are:

- i. power path insertion loss: must be low enough such that power laser requirements are not unreasonably high;
- ii. signal path isolation: must be high enough such that the power light does not significantly increase the noise at the output of the signal photodiode
- iii. power handling: must be high enough to enable adequate power to be provided for the remote unit components.

Fortunately, there are many WDM components that can meet these requirements.

III. EXPERIMENTAL SYSTEM LAYOUT

The layout of the constructed experimental WDM transmission system is shown in Fig. 1. The aim of the experiment was to investigate the impact of using WDM to

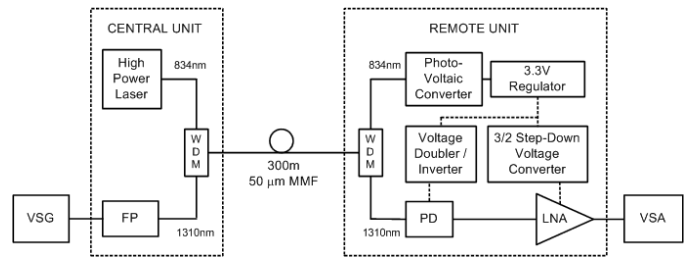


Figure 1. Experimental system layout.

combine signal and power over a single fiber; thus, the radio over fiber part was kept relatively simple (a unidirectional link with a post RF amplifier). The central unit consisted of a high power laser, signal laser (1 mW at 1310 nm into single mode fiber) and WDM multiplexer (a thin-film micro-optic device with insertion loss of 0.3 dB at 834 nm and 0.2 dB at 1310 nm).

The fiber reel consisted of 300 m of OM3 multimode fiber with a core diameter of 50 μm and insertion loss of 0.7 dB at 834 nm and 0.1 dB at 1310 nm. The relative response of this reel was -1.2 dB at 1310 nm and 2.5 GHz. The fiber length chosen for this work is representative of a real deployment scenario since around 90 % of the worldwide installed base of in-building multimode fiber is below this length [6].

The remote unit contained a WDM demultiplexer, photovoltaic converter, signal photodiode, RF amplifier, and power supply board containing a voltage regulator and voltage converters to provide power for the amplifier and photodiode [1]. The demultiplexer was the same type of device as the central unit multiplexer and had an insertion loss of 0.2 dB at 834 nm and 0.2 dB at 1310 nm. The isolation of this device was 46 dB for power light leakage into the signal path and 23 dB for signal light leakage into the power path. Power light leakage into the signal path is of great concern for a system such as this since we are dealing with very high power levels; any light leakage will increase the photocurrent, generating excess noise. However, with an isolation of 46 dB, there is no discernable increase in signal photocurrent as a result of using the optical power supply.

The remote unit amplifier was constructed using an Avago Technologies ATF-55143 transistor [10]. It was designed for 2.2 V operation, with a gain of 15 dB and a P1dB of +7 dBm at a frequency of 2.5 GHz. The power consumption of the amplifier was 20 mW (2.2 V and 9 mA) and the power consumption of the signal photodiode was 5 mW (-6.6 V and 0.75 mA). The power supply (voltage regulator and converters) had an overall efficiency of 82 %, which meant that the photovoltaic converter had to provide an electrical output power of 30 mW. The photovoltaic converter provided a 4 V output with an optical to electrical conversion efficiency of 50 %, thus an optical power of 60 mW was required at its input. The transition from 62.5 μm to 50 μm core diameter fiber between the power laser and the WDM multiplexer resulted in an additional optical loss of 2 dB.

TABLE I. POWER BUDGET FOR REMOTE POWERING

<i>Remote Unit Electrical Power</i>	
Power required for PD and amplifier	25 mW
Power supply efficiency	82 %
Total electrical power required	30 mW
<i>Remote Unit Photovoltaic converter</i>	
Efficiency	50 %
Required optical power	60 mW
<i>Fiber Losses for Power Link</i>	
62.5 μm – 50 μm transition	2 dB
WDM multiplexer	0.3 dB
300 m fiber reel	0.7 dB
WDM demultiplexer	0.2 dB
<i>Central Unit Power Laser</i>	
Required output power	125 mW

This loss is similar to the loss experienced when using optical sources that excite most of the fiber modes, such as LEDs [7], and is expected here since the power laser has an active layer width spanning the entire core of the output fiber. The total optical loss in the power transmission path including the fiber and WDM multiplexer/demultiplexer losses was therefore 3.2 dB. The power laser output was set to 125 mW in order to provide the required power at the photovoltaic converter. The power budget for the remote powering is presented in Table I.

The power handling limit of the WDM multiplexer was 300 mW, well above the optical power level used here. This limit will restrict the power available for high performance remote units, but other WDM components are commercially available with higher power handling capabilities. A multiplexer with 500mW of power handling capability would be sufficient to provide approximately 140 mW of electrical power for the remote unit, assuming losses and efficiencies similar to those encountered here. In [1] it was shown that this level of electrical power was sufficient for a remote unit with a laser, photodiode and several stages of amplification, including a downlink power amplifier with a P1dB of at least +16 dBm. The signal path (FP laser, multiplexer, fiber reel, demultiplexer and photodiode) had a total RF insertion loss of 30 dB at 2.5 GHz. The post amplifier gain was 15 dB which gave an end-to-end RF loss of 15 dB between the signal generator and signal analyzer. Characterization of the signal path was made by measuring error vector magnitude as a function of input power to the laser. Both optical and electrical power supplies (a standard bench-top power supply in place of the photovoltaic converter) were used in order to verify that there was no penalty associated with using the optical supply.

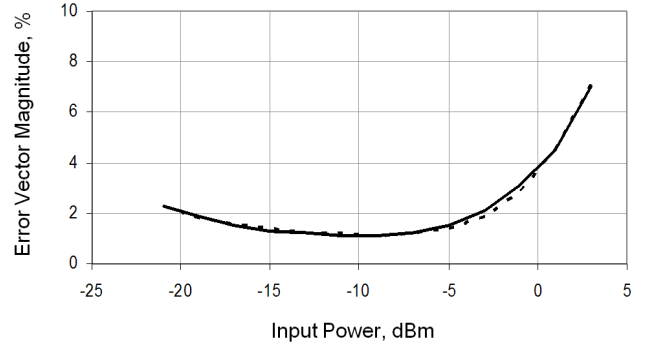


Figure 2. Error vector magnitude as a function of input power for optical (solid line) and electrical (dashed line) power supplies.

IV. TRANSMISSION MEASUREMENT RESULTS

Error vector magnitude was measured as a function of input power to the signal laser and the results are given in Fig. 2 for both optical and electrical power supplies. Transmission was at 2.5 GHz using a 64-QAM, OFDM signal with a symbol rate of 9Ms/s. These are the most demanding modulation and symbol rate parameters used in the IEEE802.11g wireless local area networking standard [10]. The EVM curve follows the expected shape; at low input power the EVM is high due to reduced signal to noise ratio and at high input power the EVM is high due to increased distortion from the laser and RF amplifier. At the optimum input power, the EVM is 1.1 % which is very low compared to the maximum allowed in the IEEE802.11g specification of 5.6 %. The transmission performance of the signal path is therefore of high quality. The most important point to note from Fig. 2 however is that there is no significant difference between the EVM curves for each type of power supply. This is because the isolation of the WDM demultiplexer is sufficient to avoid any additional noise at the output of the signal photodiode. This was verified by performing separate noise measurements at 2.5 GHz. A noise power of -119 dBm/Hz was measured for both types of power supply. For the present experimental arrangement, the additional photocurrent is calculated to be only 1.5 μA , which is insignificant compared to the signal photocurrent of 0.75 mA.

V. CONCLUSION

Wavelength division multiplexing has been used to combine signal and power transmission on a single fiber to provide an optically powered radio over fiber remote unit. The isolation of the thin-film micro-optic WDM demultiplexer used is found to be high enough to ensure that there is no impact on signal transmission performance (at the wavelengths chosen). The only impact is the higher optical power requirements for the high power laser, due to multiplexer and demultiplexer losses (a total of 0.5 dB in this case) and any additional loss incurred if a smaller core diameter transmission fiber is chosen compared to that of the power laser output fiber. In

the case described here (with a 62.5 μm / 50 μm fiber transition), an additional 2 dB power penalty is observed. With similar losses and efficiencies to those measured in this work, commercially available WDM multiplexers with at least 500mW power handling capability would be able to provide approximately 140 mW of electrical power for the remote unit.

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