



# Kent Academic Repository

Hutiu, Gheorghe, Dimb, Alexandru-Lucian, Duma, Virgil-Florin, Demian, Dorin, Bradu, Adrian and Podoleanu, Adrian G.H. (2018) *Roughness measurements using optical coherence tomography: a preliminary study*. In: Todea, Carmen C. and Podoleanu, Adrian G.H. and Duma, Virgil-Florin, eds. *Seventh International Conference on Lasers in Medicine*. Proceedings of SPIE, 19 (59). SPIE. ISBN 978-1-5106-2287-6.

## Downloaded from

<https://kar.kent.ac.uk/68715/> The University of Kent's Academic Repository KAR

## The version of record is available from

<https://doi.org/10.1117/12.2282807>

## This document version

Publisher pdf

## DOI for this version

## Licence for this version

UNSPECIFIED

## Additional information

## Versions of research works

### Versions of Record

If this version is the version of record, it is the same as the published version available on the publisher's web site. Cite as the published version.

### Author Accepted Manuscripts

If this document is identified as the Author Accepted Manuscript it is the version after peer review but before type setting, copy editing or publisher branding. Cite as Surname, Initial. (Year) 'Title of article'. To be published in *Title of Journal*, Volume and issue numbers [peer-reviewed accepted version]. Available at: DOI or URL (Accessed: date).

## Enquiries

If you have questions about this document contact [ResearchSupport@kent.ac.uk](mailto:ResearchSupport@kent.ac.uk). Please include the URL of the record in KAR. If you believe that your, or a third party's rights have been compromised through this document please see our [Take Down policy](https://www.kent.ac.uk/guides/kar-the-kent-academic-repository#policies) (available from <https://www.kent.ac.uk/guides/kar-the-kent-academic-repository#policies>).

# PROCEEDINGS OF SPIE

[SPIDigitalLibrary.org/conference-proceedings-of-spie](https://spiedigitallibrary.org/conference-proceedings-of-spie)

## Roughness measurements using optical coherence tomography: a preliminary study

Gheorghe Hutiu, Alexandru-Lucian Dimb, Virgil-Florin Duma, Dorin Demian, Adrian Bradu, et al.

Gheorghe Hutiu, Alexandru-Lucian Dimb, Virgil-Florin Duma, Dorin Demian, Adrian Bradu, Adrian Gh. Podoleanu, "Roughness measurements using optical coherence tomography: a preliminary study," Proc. SPIE 10831, Seventh International Conference on Lasers in Medicine, 108310S (10 August 2018); doi: 10.1117/12.2282807

**SPIE.**

Event: Seventh International Conference on Lasers in Medicine, 2017, Timisoara, Romania

# Roughness measurements using optical coherence tomography: A preliminary study

Gheorghe Hutiu<sup>a</sup>, Alexandru-Liviu Dimb<sup>a</sup>,  
Virgil-Florin Duma<sup>a,b\*</sup>, Dorin Demian<sup>a</sup>, Adrian Bradu<sup>c</sup>, Adrian Gh. Podoleanu<sup>c</sup>

<sup>a</sup>3OM Optomechatronics Group, *Aurel Vlaicu* University of Arad, 77 Revolutiei Ave., 310130 Arad, Romania

<sup>b</sup>Doctoral School, Polytechnic University of Timisoara, 1 Mihai Viteazu Ave., 300222 Timisoara, Romania

<sup>c</sup>Applied Optics Group, School of Physical Sciences, University of Kent, Canterbury, CT2 7NH, United Kingdom

## ABSTRACT

To determine the roughness is an important aspect in both industrial and biomedical applications. We propose and utilize for roughness evaluations, a non-destructive evaluation methods, Optical Coherence Tomography (OCT). For the metallic surfaces investigated from this point of view, the Ra and Rz parameters are utilized, according to ISO 4287/1988. Also, according to ISO 4280 and ISO 3274 standards, the measurements have been made on 12.5 mm portions. In order to accommodate such evaluations with the specific OCT field-of-view, four consecutive OCT images have been made for each sample, and an appropriate processing of the data collected from the surface profiles has been made. A validation of the results obtained with OCT has been completed with the gold standard for such evaluations, using a contact mechanical method, with a Mitutuyo profiler.

**Keywords:** Optical Coherence Tomography (OCT), roughness, metallic materials, non-contact measurements, imaging methods, handheld probes, manufacturing, dental medicine.

## 1. INTRODUCTION

The shape and dimensions of imperfections in processed parts depend on several factors, including: the processing operations, the shape of the cutting tool, the cutting cycle (particularly the cutting feed), and the manner in which the chip/splinter is formed – the latter aspect including its cycle, geometry/shape, and material.

These imperfections or profile ruggedness are standardized by ISO 11562-1996 and ISO 16610-21/1996 into the Primary Profile, the Waviness profile and the Roughness Profile. Surface profiles of processed parts bring about disadvantages, such as: a diminishing of the contact surface, an increase in wear, a decrease of the fatigue endurance limit, etc.

The measurement methods for surface roughness profiles are specified in specific standards. Thus, the ISO4287-1998 standard provides methods for determining the surface profile evolution using stylus profile meters; they register the profile along a profile length of several millimeters. ISO 4287 is part of the Geometrical Product Specifications (GPS), which also comprises the following standards: ISO 3274, ISO4287, ISO4288, ISO11562, and ISO16610-21. These standards specify the contact characteristics of the stylus, provide rules and procedures for surface certification, specify parameters defining surface roughness and filters to be used, etc.

ISO 4287 and ISO 4288 classify the parameters that define the surface evolution in the following way:

(a) Field parameters  $R_a$ ,  $R_q$ ,  $R_{sk}$ ,  $R_{ku}$ ,  $R_p$ ,  $R_v$ , and  $R_z$ ; amplitude parameter  $R_t$ ;

---

\* Email: [duma.virgil@osamember.org](mailto:duma.virgil@osamember.org); Tel.: +40-751-511451; Site: <http://3om-group-optomechatronics.ro/>

(b) Feature parameters  $R_c$  (peak-valley) and  $RS_m$  (spacing).

In order to control roughness profiles, the following methods can be used:

(a) comparative determination of roughness using roughness specimens made of steel, cast iron, etc.;

(b) quantitative determination of roughness achieved by using specialized probing equipment (profile meters, profilographs, atomic force microscope);

(c) non-contact classical optical methods and equipment (optical microscopes or interferometers);

(c) non-contact optical methods that have been less used before for such applications, like Optical Coherence Tomography (OCT) – as we explore in this study.

The latter two categories, of optical non-contact methods are currently used for the measurement of surface roughness, and they include: measurement of reflectance [1, 2]; laser speckle techniques [3-8]; two wavelength holographic interferometry [9]; reflected step edges [10]; laser measurements [11, 12]; white light interferometry [13-18]; scattering [19]; terahertz reflection spectra [20]; adaptive optics [21]; low coherence interferometry [22]; OCT based on vertical scanning interferometry (VSI) [23]; spectrophotometric measurements [24].

Comparisons between values of roughness measured through mechanical versus optical methods have been made since 1962. An “Optical Measurements Procedures Guide” was thus edited in 1988 in order to explain in simple terms how several basic optical measurements are made.

Experiments have been carried out on glass, composite materials, metallic materials (steel, aluminum, nickel, bronze, etc.). All these materials were processed through a variety of mechanical procedures like grinding, polishing, milling, belt sanding, etc. The non-contact methods have been used to determine three parameters: mean height of roughness ( $R_a$ ); root mean square height of roughness ( $R_q$ ); maximum height of roughness ( $R_z$ ).

Depending on the material analyzed and the processing operation to which it was previously submitted, the values of these parameters may vary in the Å, nm, or  $\mu\text{m}$  range.

Measurements made using optical methods have been compared with those made using for example the stylus [14, 17] and there were always variations in the parameter values measured by the stylus and those obtained by non-contact methods. The roughness of the measured surfaces in such investigations has been low (i.e.,  $R_z < 3\mu\text{m}$ ). The lengths of the surfaces analyzed by non-contact methods have been situated in the  $\mu\text{m}$  range.

The standards specifying surface roughness evaluation through mechanical methods stipulate that roughness should be determined on different length depending on the roughness of the surface: for  $R_z > 50\mu\text{m}$  – 40 mm; for  $R_z = 10\text{-}50\mu\text{m}$  – 12.5 mm; for  $R_z = 0.5\text{...}10\mu\text{m}$  – 4 mm; for  $R_z = 0.1\text{...}0.5\mu\text{m}$  – 1.25 mm; for  $R_z < 0.1\mu\text{m}$  – 0.4 mm.

## 2. MATERIALS AND METHODS

### 2.1 Samples

In the present study a steel, mechanically milled Commercial Roughness Standard has been used (Fig. 1). The nominal values of its roughness parameters have been  $R_z = 10\mu\text{m}$  and  $R_a = 2.4\mu\text{m}$ .

### 2.2. OCT System

The surface microstructures have been analyzed using an in-house developed Swept Source (SS)-OCT system with a 10  $\mu\text{m}$  resolution [25]. A Scanning Electron Microscope (SEM) system with a 4 nm resolution has been used to validate some of the OCT investigations.

The schematic diagram of the SS-OCT imaging system is similar to the one reported in [25, 26]. A SS (Axsun Technologies, Billerica, Massachusetts), with a central wavelength of 1060 nm, a sweeping range of 106 nm (quoted at 10 dB), and a 100 kHz line rate has been used. A low coherence interferometer with a balance detection receiver (Thorlabs, Newton, NJ, model PDB460C) was used, and a dual axis XY galvanometer-based scanner (Cambridge Technology, Bedford, Massachusetts, model 6115) [27] was used to scan the IR laser beam over the sample.



Figure 1. Commercial Roughness Standard with a  $R_z$  nominal value of 10  $\mu\text{m}$  and a  $R_a$  nominal value of 2.4  $\mu\text{m}$ .

### 2.3 Roughness Parameters

The parameters used to determine the surface roughness are shown in Table 1. The following well-known mathematical formulas have been used for the calculus of  $R_z$  and  $R_a$  [28]:

$$R_a = \frac{1}{n} \sum_{i=1}^n |Z_i - Z| \quad (1)$$

where  $n$  is the number of the points within a sampling length,  $Z_i$  is the height value of a point  $i$ , and  $Z$  is the arithmetic mean of  $Z_i$  within a sampling length:

$$R_z = Z_p - Z_v, \quad (2)$$

where  $Z_p$  is the largest profile peak height and  $Z_v$  is the largest profile valley depth within a sampling length.

Table 1. Roughness parameters.

Parameters	Specific standard	Definition
$R_a$	ISO 4287/1998	Arithmetic average deviation of the profile
$R_z$	ISO 4287/1998	Maximum height of the assessed profile

### 2.4 Applying the OCT method

The Commercial Roughness Standard shown in Fig. 1 has been investigated using the SS-OCT system in order to determine the roughness parameters  $R_a$  and  $R_z$ . According to ISO 4288 and ISO 3274, the measurements for a value of  $R_z$  of 10  $\mu\text{m}$  have to be made along a length of 12.5 mm. For this Commercial Roughness Standard with  $R_z$  equal to 10  $\mu\text{m}$ , several consecutive scans have been made, and the corresponding OCT images have been obtained. The area of the scanned surface has been 3.125 x 3.125 mm and 1000 OCT B-scans (cross-section, i.e., height profiles) were performed on this surface, each of the B-scans having 1000 points.

### 2.5 The procedure used to determine Roughness Parameters from OCT B-scans

In order to determine the value of parameters  $R_z$  and  $R_a$ , the processing of the B-scans obtained using OCT has been performed using ImageJ, Matlab, and Excel.

For this Commercial Roughness Standard with the nominal value  $R_z$  equal to  $10\ \mu\text{m}$  several B-scans have been analyzed: 1, 250, 500, 750, and 988 (somehow equally spaced B-scans on the surface of the sample, out of the total of 1000 B-scans). An illustration of one of these analyses is given in Fig. 2 - for the B-scan 250. After scanning, the B-scans have been imported in Matlab; using this, the values of the coordinates  $x$  and  $y$  have been determined for each of the 1000 points of the B-scan. The  $x$  and  $y$  coordinates obtained using Matlab have then been transferred to Excel – Fig. 3, where the graph ( $x, f(y)$ ) has been plotted.

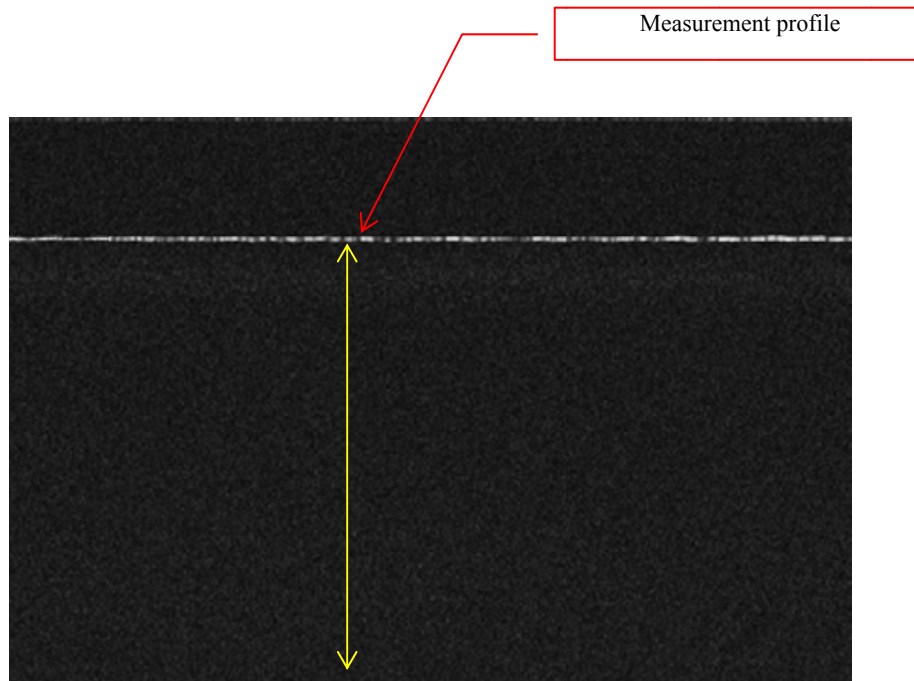


Figure 2. OCT B-scan number 250 – considered in order to determine the values of  $R_{z5}$  and  $R_{a5}$

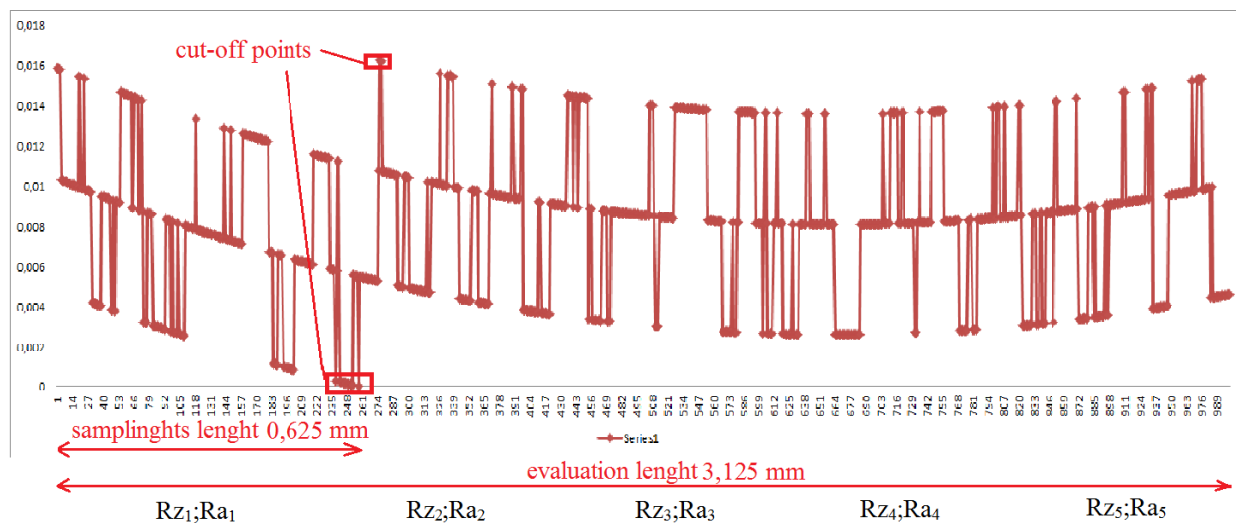


Figure 3. Graph of the measured values of the height profile for the B-scan number 250.

## 2.6. Determining $R_z$ and $R_a$ for the Commercial Roughness Standard with $R_z$ of 10 $\mu\text{m}$ and $R_a$ of 2.4 $\mu\text{m}$

The B-scans 1, 250, 500, 750, and 998 have been processed using ImageJ, Matlab and Excel in accordance with the steps described in section 2.5.

Four consecutive scans have been carried out on the commercial Roughness Standard using OCT. After each scan the five B-scans mentioned have been analyzed.

Tables 2 and 3 show the results of these OCT B-scans, processed, i.e. the values of the parameters  $R_z$  and  $R_a$ .

Table 2.  $R_z$  values obtained using OCT.

B-scan	1	250	500	750	998	Average
Nr.						
1	12.66	13.32	12.07	12.91	12.06	<b>12.60</b>
2	12.33	11.96	12.34	14.94	12.63	<b>12.84</b>
3	12.46	12.28	13.54	12.36	13.31	<b>12.79</b>
4	13.79	13.11	13.16	11.85	12.83	<b>12.94</b>
Average	<b>12.81</b>	<b>12.66</b>	<b>12.77</b>	<b>13.01</b>	<b>12.70</b>	

The average value of  $R_z$  for a B-scan ranges between 12.66  $\mu\text{m}$  and 13.01  $\mu\text{m}$ , while the average value of the five B-scans is 12.79  $\mu\text{m}$ .

Table 3.  $R_a$  values obtained using OCT

B-scan	1	250	500	750	998	Average
Nr.						
1	2.84	2.95	2.97	2.73	2.66	<b>2.83</b>
2	2.86	2.82	2.81	3.20	3.08	<b>2.95</b>
3	3.04	2.72	3.16	3.03	3.13	<b>3.01</b>
4	3.05	3.04	2.98	2.80	3.18	<b>3.01</b>
Average	<b>2.94</b>	<b>2.88</b>	<b>2.98</b>	<b>2.94</b>	<b>3.01</b>	

The average value of  $R_a$  for a B-scan ranges between 2.94  $\mu\text{m}$  and 3.01  $\mu\text{m}$ , and the average value of the five B-scans is 2.95  $\mu\text{m}$ .

## 3. CONCLUSIONS

The average  $R_z$  value measured by the OCT is 12.79  $\mu\text{m}$ , with 27.9% bigger than the  $R_z$  value of the Commercial Roughness Standard (10  $\mu\text{m}$ ), while the  $R_a$  value is 2.95  $\mu\text{m}$ , with 22.91 % bigger than the  $R_a$  value of the Commercial Roughness Standard (2.4  $\mu\text{m}$ ).

The following remarks can be made: (i) If we consider B-scans 1, 250, 500 performed on the four scans, the average values obtained are an average  $R_z$  of 12.74  $\mu\text{m}$  and an average  $R_a$  of 2.93  $\mu\text{m}$ ; (ii) If we consider B-scans 1, 250, 750 performed on the four scans, the values obtained are an average  $R_z$  of 12.82  $\mu\text{m}$  and an average  $R_a$  2.92  $\mu\text{m}$ ; (iii) If we consider B-scans 1, 250, 998 performed on the four scans, the values obtained are an average  $R_z$  of 12.72  $\mu\text{m}$  and an

average  $R_a$  2.94  $\mu\text{m}$ ; (iv) If we consider B-scans 250, 500, 750 performed on the four scans, the values obtained are an average  $R_z$  of 12.81  $\mu\text{m}$  and an average  $R_a$  2.93  $\mu\text{m}$ ; (v) If we consider B-scans 250, 500, 998 performed on the four scans, the values obtained are an average  $R_z$  of 12.71  $\mu\text{m}$  and an average  $R_a$  of 2.95  $\mu\text{m}$ ; (vi) If we consider B-scans 500, 750, 998 performed on the four scans, the values obtained are an average  $R_z$  of 12.82  $\mu\text{m}$  and an average  $R_a$  of 2.97  $\mu\text{m}$ .

The conclusion is that in the cases when the measurements are carried out on three B-scans, the values of  $R_z$  and  $R_a$  are close to the values obtained on the five B-scans. However, if only the first scan of 3.125 mm is taken into account, there are significant differences between the  $R_z$  and  $R_a$  values measured using OCT and those of the Commercial Roughness Standards. In order to obtain the  $R_z$  and  $R_a$  values closer to the Commercial Roughness Standard values, the scanned length has to be 12.5 mm – which confirms the standards in use, according to ISO 4288/1988.

## ACKNOWLEDGMENTS

This work is supported by the Romanian National Authority for Scientific Research, CNDI–UEFISCDI project PN-III-P2-2.1-PTE-2016-0181 (<http://3om-group-optomechatronics.ro/>).

## REFERENCES

- [1] Depew, C. A. and Weir, R. D., “Surface Roughness Determination by the Measurement of Reflectance,” *Applied Optics* **10**(4) 969-970 (1971).
- [2] Creath, K. and Wyant, C. “Absolute measurement of surface roughness,” *Applied Optics* **29**(26), 3823-3827 (1990).
- [3] Sprague, R.A., “Surface Roughness Measurement Using White Light Speckle,” *Applied Optics* **11**(12), 2811-2816 (1972).
- [4] Fujii, H. and Shindo, Y., “Measurements of surface roughness properties by means of laser speckle techniques,” *Optics Communications* **16**(1), 68-72 (1976).
- [5] Fujii, H. and Lit, J. W. Y., “Surface roughness measurement using dichromatic speckle pattern: an experimental study,” *Applied Optics* **17**(17), 2690-2694 (1978).
- [6] Russo, N. A. and Sicre, E., “Real-time measurement of surface roughness through Young's fringes modulated speckle,” *Applied Optics* **31**(22), 4334-4336 (1992).
- [7] Tay, C. J., Toh, S. L., Shang, H. M., Zhang, J. B., “Whole field measurement of surface roughness using laser speckle,” *Journal of Materials Processing Technology* **38**, 195-202 (1993).
- [8] Hamed, A.M., El-Ghandoor, H., El-Diasty, F., and Saudy, M., “Analysis of speckle images to assess surface roughness,” *Optics & Laser Technology* **36**, 249 – 253 (2004).
- [9] Ribbens, W. B., “Surface Roughness Measurement by Two Wavelength Holographic Interferometry,” *Applied Optics* **13**(5), 1085-1088 (1974).
- [10] Stone, R. A. and Shafer, S. A., “Determination of surface roughness from reflected step edges,” *J. Opt. Soc. Am. A* **11**(11), 2969-2980 (1994).
- [11] Whitley, J. Q., Kusy, R. P., Mayhew, M. J., and Buckthal, J. E., “Surface roughness of stainless steel and electroformed nickel standards using a HeNe laser”, *Optics and Laser Technology* **19**(4), 189-196 (1987).
- [12] Oh, J.-S. and Kim, S.-W., “Femtosecond laser pulses for surface-profile metrology,” *Optics Letters* **30**(19), 2650-2652 (2005).
- [13] de Groot, P. and Colonna de Lega, X., “Signal modeling for low-coherence height-scanning interference microscopy,” *Applied Optics* **43**(25), 4821-4830 (2004).
- [14] Hering, M., Körner, K., and Jähne, B., “Correlated speckle noise in white-light interferometry: theoretical analysis of measurement uncertainty,” *Applied Optics* **48**(3), 525-538 (2009).
- [15] Lehmann, P., “Vertical scanning white-light interference microscopy on curved microstructures,” *Optics Letters* **35**(11), 1768-1770 (2010).
- [16] Pavlíček, P. and Häusle, G., “White-light interferometer with dispersion: an accurate fiber-optic sensor for the measurement of distance,” *Applied Optics* **44**(15), 2978-2983 (2005).
- [17] Laopornpichayanuwat, W., Visessamit, J., and Tianprateep, M., “3-D surface roughness profile of 316-stainless steel using vertical scanning interferometry with a superluminescent diode,” *Measurement* **45**(10), 2400-2406 (2012).



- [18] Zerrad, M., Deumié, C., Lequime, M., and Amra, C., "An alternative scattering method to characterize surface roughness from transparent substrates," *Optics Express* **15**(15), 9222-9231 (2007).
- [19] Jagannathan, A., Gatesman, A. J., and Giles, R. H., "Characterization of roughness parameters of metallic surfaces using terahertz reflection spectra," *Optics Letters* **34**(13), 1297-1299 (2009).
- [20] Fuh, Y. K., Hsu, K. C., and Fan, J. R., "Rapid in-process measurement of surface roughness using adaptive optics," *Optics Letters* **37**(5), 848-850 (2012).
- [21] Onodera, R., Wakaumi, H., and Ishii, Y., "Measurement technique for surface profiling in low coherence interferometry," *Optics Communication* **254**, 52-57 (2005).
- [22] Xie, W., Lehmann, P., and Niehues, J., "Lateral resolution and transfer characteristics of vertical scanning white-light interferometers," *Applied Optics* **51**(11), 1795-1803 (2012).
- [23] Guo, C., Kong, M., Gao, W., Li, B., "Simultaneous determination of optical constant thickness, and surface roughness for thin film from spectrophotometric measurements," *Optics Letters* **38**(1), 40-42 (2013).
- [24] Podoleanu, A.Gh. and Bradu, A., "Master-slave interferometry for parallel spectral domain interferometry sensing and versatile 3D optical coherence tomography," *Optics Express* **21**, 19324-19338 (2013).
- [25] Hutiu, Gh., Duma, V.-F., Demian, D., Bradu, A., and Podoleanu, A. Gh., "Surface imaging of metallic material fractures using optical coherence tomography," *Applied Optics* **53**(26), 5912-5916 (2014).
- [26] Duma, V.-F., Tankam, P., Huang, J., Won, J. J., and Rolland, J. P., "Optimization of galvanometer scanning for Optical Coherence Tomography," *Applied Optics* **54**, 5495-5507 (2015).
- [27] ISO-4287/1998; 3274/1996; 4288/1996; 11562/1996; 16610-21/1996.