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1  
2 **Biometric variables predict stone tool functional performance more effectively**  
3 **than tool-form attributes: a case study in handaxe loading capabilities**  
4

5  
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11

12 **Abstract**

13 Both the form of a stone tool, and the anatomy of the individual using it, have potential to  
14 influence its cutting performance. To date, however, the selective pressures acting on stone-  
15 tool form and hominin biometric/biomechanical attributes have been investigated in isolation  
16 and their relative influence on performance have never been compared directly. Here, we  
17 examine the influence of both tool-form attributes and biometric variation on the functional  
18 performance of Acheulean handaxes. Specifically, we investigate the impact of 13 tool  
19 attributes and eight biometric traits on the working forces applied through the edge of 457  
20 replica tools. The relative contribution of tool-form and biometric attributes to handaxe loading  
21 levels were examined statistically. Results identify that both tool-form attributes and biometric  
22 traits are significantly related to loading, however, tool-user biometric variation has a  
23 substantially greater impact relative to tool-form attributes. This difference was demonstrated  
24 by up to a factor of ten. These results bear directly on the co-evolutionary relationships of stone  
25 tools and hominin anatomy, and the comparative strength of selective pressure acting on each.  
26 They also underline why handaxe forms may have been free to vary in form across time and  
27 space without necessarily incurring critical impacts on their functional capabilities.  
28

29 **Keywords:** Acheulean; ergonomics; cutting force; biface, Lower Palaeolithic, selective  
30 pressure

## 31 **1. Introduction**

32 Archaeologists and anthropologists often seek to reconstruct how efficiently lithic artefacts  
33 could have been used by Plio-Pleistocene hominins (Schick and Toth, 1993; Shea, 2007;  
34 Marzke, 2013; Key and Lycett, 2017a). Two analytical routes are typically used to investigate  
35 this. The first examines the morphology of stone tools recovered from the archaeological record  
36 and interprets how efficiently or effectively they could have been used during cutting tasks.  
37 The second relies on reconstructing the biomechanical capabilities and comparative tool-use  
38 abilities of fossil hominins. Beyond the invaluable data derived from artefact and fossil  
39 morphologies, both routes rely heavily on experimental programs undertaken using modern  
40 human subjects.

41 Experimental research over the past 40 years has, for example, demonstrated that the  
42 performance characteristics (*sensu* Schiffer and Skibo, 1997) of flake stone tools are influenced  
43 by their size, edge morphology and sharpness (Walker, 1978; Jobson, 1986; Prasciunas, 2007;  
44 Key and Lycett, 2014, 2015; Key et al., 2018). Others have demonstrated that edge curvature  
45 and regularity influence the performance of scraping tools (Collins, 2008; Clarkson et al.,  
46 2015), while size, edge angle, and potentially symmetry, can influence the functional  
47 capabilities of Acheulean bifaces (Jones, 1981; Machin et al., 2007; Key et al. 2016; Key and  
48 Lycett, 2017b). In other words, it has been demonstrated that some tool-form attributes can  
49 have a strong and statistically significant impact on a stone tool's performance characteristics.

50 Similarly, experimental data have demonstrated that an individual's biomechanical  
51 capabilities and biometric traits can impact the efficiency and effectiveness of stone tool use.  
52 Marzke and Shackley (1986) were among the first to demonstrate how anatomical features of  
53 the hand, including a strong, relatively long thumb were linked to the performance of hand-  
54 held stone tools. Key and Lycett (2018) have more recently demonstrated how the strength and  
55 dimensions of tool user's hands are correlated with the cutting performance of flake tools and  
56 handaxes, with different biometric traits contributing to tool efficiency in variable ways  
57 dependent on the type of tool used. Rolian et al. (2011) also demonstrated a negative  
58 relationship between the length of a tool user's digits and the muscular force required to  
59 stabilize joints during 'simulated stone tool use'. Work by Hamrick et al. (1998) and Williams-  
60 Hatala et al (2018) further emphasizes the high muscular recruitment and loading required by  
61 the thumb and index finger during effective flake and handaxe use. Other work has examined

62 fossil evidence, with the aim of identifying the influence that stone tool production and use  
63 likely had on hominin manual anatomy (Marzke, 1997, 2013; Kivell, 2015).

64         Given such work, it is now well established that both the form of a stone tool and the  
65 biometric traits of the individual using it can influence its functional performance. Both types  
66 of variable affect performance via their influence on ‘cutting stress’, which is created in a  
67 worked material by the tool’s cutting edge (Atkins 2009). Cutting stress, calculated as force  
68 per unit area ( $\sigma = N/m^2$ ), dictates whether an edge can create a fracture (i.e. cut) in a worked  
69 material. The greater the stress, the more likely it is that material bonds will be broken (Atkins  
70 2009). The morphology of a stone tool’s cutting edges (e.g. edge radii, angle, curvature)  
71 influence cutting stress by altering the amount (area) and morphology of the edge in contact  
72 with the material being cut and, moreover, how forces are distributed through this edge  
73 (Ackerly, 1978; Atkins, 2009; Key, 2016). Overall tool-size and shape attributes, meanwhile,  
74 affect the ergonomic nature of the tool, how precisely it may be applied during cutting, and  
75 how much force is required to stabilize the tool in the hand, as well as the length of utilizable  
76 cutting edge (Jones, 1981; Hall, 1997; Seo and Armstrong, 2008; Toth and Schick, 2009; Rossi  
77 et al., 2014; Wynn and Gowlett, 2018; Key et al., in press). The biomechanical capabilities of  
78 tool users may similarly impact force application, tool stabilisation and movement, and cutting  
79 precision. This can be realized through the amount of muscular force created by the tool user  
80 and transferred through joint surfaces, which in turn, changes the forces conveyed through the  
81 tool and onto the worked material. Alternatively, there can be variation in the opposability of  
82 manual aspects and the ease with which tools can be securely gripped when resisting use-  
83 related forces, or when rotating and manipulating tools (Marzke and Shackley, 1986; Rolian et  
84 al., 2011; Seo and Armstrong, 2008; Key and Lycett, 2018).

85         An understanding of how the working-force capabilities of stone tools is influenced by  
86 independent variables are, then, essential to understanding how they create cutting stress and  
87 their eventual efficiency during use. In particular, the performance attribute of ‘loading’ (i.e.,  
88 the creation of force normal and parallel to the worked material) and its role in the creation of  
89 cutting stress is a parameter that is key to understanding the relative efficacy of prehistoric  
90 cutting tools (Atkins, 2009), including butchery processes, woodworking, digging for tubers,  
91 scraping hides, among others. Indeed, functional interpretations of individual morphological  
92 traits in an absence of their known influence on force creation, diminishes our understanding  
93 of that cutting tool’s potential performance or capabilities.

94           If, as is often argued (Jones, 1981; Isaac, 1981; Shea, 2007; Key and Lycett, 2017a),  
95 the functional performance of stone cutting tools was of concern to Plio-Pleistocene hominins  
96 and had potential to impact resource acquisition, survival and—ultimately—reproductive  
97 success, then variables facilitating greater cutting stress could have been positively selected  
98 for. Given the foregoing, this could have been achieved through selection on hominin  
99 biomechanical attributes and/or on tool forms. Indeed, it has been argued that functional  
100 selective pressures were likely influencing the form of lithic artefacts produced by Plio-  
101 Pleistocene hominins (e.g. Crompton and Gowlett, 1993; Diez-Martín et al., 2014; Borel et al.,  
102 2017; Key and Lycett, 2017a; Wynn and Gowlett, 2018). Moreover, effective and efficient  
103 stone tool use requirements are widely thought to have affected the evolutionary trajectory of  
104 hominin hand anatomy during this period (Marzke and Shackley, 1986; Marzke, 1997, 2013;  
105 Hamrick et al., 1998; Kivell, 2015; Rolian et al., 2011; Key and Lycett, 2018; Williams-Hatala  
106 et al., 2018). Previous investigations into the role of loading on stone tool performance have  
107 principally been focused on projectile velocities and consequences of impact (Hutchings, 2011;  
108 Milks et al., 2016), the pressures and forces distributed through tool-users’ digits (Rolian et al.,  
109 2011; Williams-Hatala et al., 2018), and the use of force sensitive cells beneath portions of cut  
110 material (Key and Lycett, 2014, 2015). To date, however, the selective pressures acting on tool-  
111 form and biometric/biomechanical attributes have been investigated in isolation and their  
112 relative strength of influence have never been compared directly.

113           This study aims to investigate the relative influence of biometric variation and tool-  
114 form variation on the loading capabilities of Acheulean handaxes. An understanding of the  
115 comparative influence of both artefactual and biological variables on stone tool performance  
116 can help to identify the relative strength of forces acting on evolutionary changes in both  
117 hominins and tools. Furthermore, such data can aid our understanding of how free biological  
118 and cultural elements were to vary without there being critical implications for the functional  
119 performance of stone implements. In turn, such considerations are important when interpreting  
120 morphological variation in fossil hominin upper limb anatomy and the Palaeolithic  
121 archaeological record. If biometric traits are determined to be significantly more influential  
122 than tool-form attributes, for example, it could be hypothesized that any variation observed in  
123 handaxes is relatively arbitrary in terms of predicting their functional capabilities, with hominin  
124 anatomy being the more critical factor. Here, we examine the influence of variation in both  
125 tool-form attributes and biometric traits on the loading capabilities of 457 replica Acheulean  
126 handaxes. Specifically, we investigate how the working forces applied through the cutting

127 edges of these replica bifaces are influenced by 13 tool-form attributes and eight biometric  
128 traits on a comparative basis.

129

## 130 **2. Materials and methods**

### 131 **2.1 Participants and Biometric Traits**

132 Participants were sourced from the student population at the University of Kent. A total of  
133 46 participants were recruited, with a female-to-male ratio of 9:14. Each individual had eight  
134 biometric traits recorded on their dominant hand. Using digital calipers, ‘Hand Length’ was  
135 recorded in millimetres (mm) from the tip of the third digit to the first (most proximal) crease  
136 line at the wrist. The ‘Digit Length’ of the thumb, index and middle fingers were similarly  
137 recorded using digital calipers from the tip of each respective digit to the inferior crease line at  
138 its intersection with the hand. First-to-second digit ratios (‘1D:2D’) were calculated for all  
139 participants by dividing the first digit length by the second. ‘Grip Strength’ was recorded in a  
140 transverse hook grip, in kilograms (kg), using a hand dynamometer. ‘Pad-to-Side Pinch  
141 Strength’, where the participant’s distal palmar aspect of the thumb opposed the lateral side of  
142 the 2nd digit, was recorded using a hydraulic pinch gauge (kg). ‘Tip-to-tip Pinch Strength’ was  
143 recorded using the same gauge (kg), with the participant’s distal palmar aspects of digits one  
144 and two forcefully opposing. Descriptive statistics for all biometric traits are detailed in Table  
145 1. Participants provided informed consent and were aware of the task conditions, items  
146 involved and general theme of the research before taking part. Participants were not aware of  
147 the specific hypotheses under investigation.

148

### 149 **2.2 Replica Handaxe Assemblage and Tool Form Attributes**

150 The replica handaxe assemblage was produced by AK (480) and SL (20) using flint sourced  
151 from Suffolk and Kent (UK). Hard and soft (antler) hammer percussion were used. In total,  
152 500 handaxes were produced, with each of the 46 participants being randomly assigned 10  
153 handaxes that were used in a randomized order, with an original intention to use a total sample  
154 of 460 handaxes for the experiment. However, due to participant #13 having to cease their  
155 participation in the experiment unexpectedly early, they only used seven handaxes, meaning  
156 that the final utilized assemblage consisted of 457 replica tools (Fig. 1).

157 Detailed below are the 13 morphological attributes recorded from each tool. In all instances,  
158 the superior surface is defined as the face displaying the largest number of flake scars above 5  
159 mm<sup>2</sup> (Lycett et al., 2006).

- 160 • ‘Mass’ was recorded in grams using digital scales.
- 161 • ‘Length’ was recorded in mm using digital calipers and was defined as the maximum  
162 distance measured on a handaxe when viewed from the superior surface.
- 163 • ‘Width’ was defined as the maximum distance between the two lateral edges of a  
164 handaxe on the superior surface when directly perpendicular to its line of maximum  
165 symmetry (see below), and was recorded in mm using digital calipers.
- 166 • ‘Thickness’ was recorded in mm using digital spreading calipers and was defined as  
167 the maximum depth of a handaxe at any point perpendicular to both Length and Width.
- 168 • ‘Shape’ was examined using a size-adjusted (scale-free) dataset of 29 morphometric  
169 variables recorded from plan and side view photos of each handaxe (following: Lycett  
170 et al., 2006). Using these metrics, Principal Component Analysis was used to describe  
171 the major patterns in shape variation within the assemblage. Here, shape is defined by  
172 PC1.
- 173 • ‘Position of Maximum Width’ was calculated as the position at which Width was  
174 recorded longitudinally on each tool, expressed as a percentage of Length (from tip  
175 [0%] to base [100%]).
- 176 • ‘Position of Maximum Thickness’ was calculated as the position at which Thickness  
177 was recorded longitudinally on each tool, expressed as a percentage of Length (from  
178 tip [0%] to base [100%]).
- 179 • ‘Width/Length’ (‘Elongation’) was calculated by dividing the aforementioned Width  
180 measurement by Length.
- 181 • ‘Thickness/Width’ (‘Refinement’) was calculated by dividing the aforementioned  
182 Thickness measurement by Width.
- 183 • ‘Percentage of Edge Flaked’ is a scale-free measurement of how much of a tool’s  
184 circumference (when in plan view) displayed a sharp, flaked edge. This was achieved  
185 by uploading an image of each tool’s superior surface into the freeware Image J. Once  
186 the scale was set, the ‘freehand’ draw and ‘measure’ functions were used to record  
187 both the total circumference of the tool’s edge and the length of flaked edge, from  
188 which the Percentage of Flaked Edge could be calculated.

- 189 • ‘Edge Uniformity’ is a measure of edge irregularity as it undulates from the tip of a  
 190 handaxe to its base. A side-profile image of each handaxe was uploaded into ‘Image  
 191 J’, from which, two measurements were taken. The first recorded the length of a  
 192 straight line between the two distal ends of the cutting edge. The second measures the  
 193 true length of the edge as it tracks up and down from the tool’s tip to its base. Straight  
 194 line length is then divided by the true length of the edge, to create a value between 0-  
 195 1 describing Edge Uniformity.
- 196 • ‘Edge Angle’ is a record of the angle produced between the two intersecting surfaces  
 197 of a biface as they join to form an edge. Edge angles from 20 locations on each tool  
 198 (tip, base, and at 10% intervals of length on both lateral edges) were recorded using  
 199 the ‘caliper technique’ (Dibble and Bernard, 1980), with the mean of these being used  
 200 as the overall measure of Edge Angle. Angles were only recorded from flaked edges  
 201 (i.e. not from those retaining cortex).
- 202 • ‘Bilateral Symmetry’ is a measure of handaxe symmetry between the two lateral sides  
 203 of a tool (recorded across a tool’s longitudinal midline). It was calculated here using  
 204 the ‘Index of Symmetry’ outlined by Lycett et al. (2006), where the distal (tip) end of  
 205 the line used to record Length is used as a locked landmark and a straight line with  
 206 equal maximum distances from the left and right edges of the tool is drawn, with this  
 207 being the line of symmetry. Perpendicular distances from this line to the left and right  
 208 edges of each handaxe were then recorded at 10% intervals of the line’s length.  
 209 Counterpart left and right measurements were used to calculate the symmetry index  
 210 using the following equation :

$$S = \sum_{i=1}^n \left( \sqrt{\frac{(x_i - y_i)^2}{(x_i + y_i)}} \right),$$

212 where  $x_i$  equals the width left of the maximum symmetry line and  $y_i$  corresponds to the  
 213 width right of the line. An index value of zero would describe complete symmetry,  
 214 while higher values quantify relative levels of deviation from perfect symmetry. The  
 215 sum of the nine individual measures of symmetry was averaged.  
 216

217 These metrics have previously been linked with the functional performance of handaxes  
 218 during cutting tasks (Jones, 1981; Gowlett, 2006, 2013; Machin et al., 2007; Grosman et al.,  
 219 2011; Key and Lycett, 2017a). Descriptive statistics for all metrics are presented in Table 2.



220

### 221 **2.3 Experimental Task**

222 Previous experimental research investigating the loading capabilities of hand-held stone tools  
223 recorded normal force (kgf) during linear cutting actions (Key and Lycett, 2014, 2015).  
224 Experimental research inevitably involves some trade-off between realism and the extent of  
225 imposed experimental controls, which are necessary for scientific rigor, but which invariably  
226 impinge on realism (Eren et al. 2016). Determining a reasonable strategy to negotiate these  
227 opposing strengths and weaknesses, must primarily be based on the specifics of the questions  
228 being addressed in any given case. Given the aims of the present research, we deliberately used  
229 an experimental task that was absent of ‘slicing’ (c.f. Atkins et al., 2004) to more precisely  
230 focus on tool-user and tool-morphology interactions and how they specifically impact on  
231 loading force levels, rather than using a task that involved cutting motions or involved the  
232 dynamics of interaction between the tool and material being cut.

233 To this end, we used a hinged wooden platform similar to that used in previous stone-tool  
234 loading research (Key and Lycett, 2014; Stemp et al., 2015). This was comprised of an upper  
235 wooden board suspended horizontally, above a lower, larger wooden board (Fig. 2). The upper  
236 board was attached to the lower via a hinge at one end, while the other end had a hard rubber  
237 stud suspended beneath it. The rubber stud rested directly on top of a Tekscan ELF Force  
238 System™ sensor. Opposing the rubber stud, on the superior side of the wooden board, was a  
239 metal bolt nut (10 mm in diameter). The metal nut was the point of contact between the handaxe  
240 and the loading platform (Fig. 2). Hence, when tool users applied force through a handaxe’s  
241 edge, they did so onto the metal bolt, with this force being transferred directly through the  
242 rubber stud and onto the force sensor. Force was recorded here in kilogram-force (1 kgf = ~9.8  
243 N) at a rate of 20Hz. The greatest force recorded during any loading event was used as the  
244 representative datum for that loading event. Loads were applied for 3-5 second periods.  
245 Participants were asked to apply as great a load as possible through the handaxe and onto the  
246 metal bolt.

247 One of the benefits of this protocol is the ability to directly control where loads are applied  
248 along the cutting edge of a handaxe, something not possible in standard cutting tasks. To this  
249 end, participants exerted force through five distinct points along the edge of each tool. These  
250 were determined by percentage intervals at 0-5%, 20%, 40%, 60% and 80% of a handaxe’s  
251 length. The mean of the five recorded forces were used here as a record of the force (kgf)

252 applied by participants through the edge of each tool. The order that percentile points along the  
253 edge were used was randomly assigned for each participant using [www.randomizer.org](http://www.randomizer.org). This  
254 prevented any potential confounding influence from fatigue.

255 Due to the potential influence that the body's position can have on loading levels during  
256 tool use (McGorry et al., 2004) the force platform was placed on a desk in front of participants  
257 while they were seated. To ensure this position was consistent, all participants adjusted the  
258 height of the chair so that their navel was level with the top of the desk, their non-dominant  
259 hand was placed on the desk next to the lower board and both feet were kept on the floor at all  
260 times. Participants were directed not to rise from a seated position at any point. Should any of  
261 these requirements be broken, participants were required to cease exerting force and the tool  
262 was re-applied. While this is not a body position likely to have regularly been used by handaxe  
263 wielding Plio-Pleistocene hominins, it does appropriately focus data collection on the loading  
264 levels achievable by the upper limb of hominins, while minimizing body mass differences and  
265 cutting-motion variation among participants.

266 The available ergonomic literature provides evidence of links between the grips used to  
267 secure a hand-held tool and subsequent achievable working loads and gripping forces (Hall,  
268 1997; Seo and Armstrong, 2008; Rossi et al., 2014). In turn, additional points of task  
269 standardization were imposed. Following previously published analyses of grip variation  
270 during the use of handaxes (Marzke and Shackley, 1986; Key et al., in press), all participants  
271 were limited to using grips where the thumb and fingers secured the handaxe on opposing sides  
272 of the tool and contact point between the palm and handaxe may go no further than 50% of the  
273 handaxe's length away from the tool's base (Fig 3). Participants were permitted to balance their  
274 index finger on the upper edge of the handaxe if they preferred (Fig. 3b, 3c). Several types and  
275 variants of grips conform to these restrictions, which together account for upwards of 85% of  
276 manual positions used during handaxe use (Key et al., in press). Particularly small handaxes  
277 were able to be held with a pad-to-side precision grip (Marzke and Shackley, 1986; Key et al.,  
278 in press). All handaxes, no matter how large, were required to be held with a single (dominant)  
279 hand. Grips were free to vary when loading different edge point locations, so long as the above  
280 conditions were met. Since participants were only applying force during the experiment rather  
281 than using the handaxes in an actual cutting motion, they were not required to use gloves.  
282 However, all participants were informed that should they experience any discomfort, they must  
283 cease tool loading immediately.

284

## 285 **2.4 Statistical Analysis**

286 Backwards stepwise regression (BSR) was used to identify which of the eight biometric and  
287 13 tool-form attributes contributed proportionately more towards the prediction of loading  
288 forces in handaxes, relative to other variables. First, a BSR was run with all 21 variables, before  
289 being repeated independently for just the eight biometric and 13 tool-form attributes. BSR  
290 begins by placing all predictors (biometric and tool-form traits) into a regression analysis and  
291 calculates the contribution of each to the model's prediction of force. If a variable is not making  
292 a significant contribution to the model then it is removed and the model is re-estimated with  
293 the remaining predictors. This continues on a stepwise basis until only variables that make a  
294 significant contribution to the model's prediction remain. Effectively, an 'order of contribution'  
295 is produced, with  $R^2$  values indicating the relative strength of relationships between  
296 independent variables and handaxe forces. Stepping criteria used entry and removal values of  
297 0.001 and 0.005, respectively. These low criteria values allowed the production of an order of  
298 contribution despite a relatively large number of variables potentially displaying a significant  
299 relationship with loading levels. In effect, forced BSR models were run.

300 The three most important biometric traits and tool-form attributes to the determination  
301 of handaxe loading capabilities, as determined by the stepwise regressions, were investigated  
302 using standard linear regression. These regressions were run to establish the predictive  
303 (explanative) power of each variable, and whether, independently, they significantly influenced  
304 the force applied by tool users. Essentially, the production of these independent linear  
305 regressions allowed assessment of the predictive power of individual traits irrespective of when  
306 removed from the BSR, as their early (forced) removal from the model may obfuscate their  
307 independent predictive power. Individual  $R^2$  values were then compared between tests to  
308 establish whether biometric or tool-form variables are more important to the determination of  
309 handaxe working force. Significance was determined in accordance with the Bonferroni  
310 Correction for multiple tests, such that  $\alpha = .008$ .

311

## 312 **3. Results**

313 Across all 457 handaxes, a mean maximum force of 3.84 kgf was recorded. There was,  
314 however, substantial variation in the forces recorded, with standard deviation equalling 4.10

315 kgf and the coefficient of variation, expressed as a percentage, equalling 107 %. Loading  
316 ranged from 0.33 kgf (~ 3.2 N) to 24.24 kgf (~ 237.7 N). In short, there was substantial variation  
317 in the forces applied through a handaxe's cutting edge, but across all participants these  
318 averaged around 4 kgf (~ 39.2 N).

319 Table 3 details the results of the BSR containing the eight biometric traits and 13 tool-form  
320 attributes. The five strongest predictive variables of handaxe loading are biometric traits, with  
321 the final stepwise model (model 20) containing both Grip Strength and Pad-to-Side Pinch  
322 Strength (despite the low entry and removal criteria). Not only does this indicate the biometric  
323 traits of tool users to be the most important criteria in the determination of handaxe working  
324 loads, but the relative strength, and in particular precision pinching strength, of tool users are  
325 the most important traits. First-to-second digit ratio, and the respective length of the first and  
326 second digits are, respectively, the third, fourth and fifth strongest predictors of force. Edge  
327 Angle makes the sixth greatest contribution towards the prediction of handaxe loading levels,  
328 and is the strongest predictive variable of all tool-form attributes. The first nine variables  
329 removed from the model are all tool-form attributes, indicating that a broad range of these  
330 variables have little to no influence on handaxe loading levels.

331 The entry of all eight biometric variables into a BSR produced 7 model steps, with two  
332 predictive variables remaining in the final model, despite the very low entry and removal  
333 criteria (Supplementary Table 1).  $R^2$  values indicate that when modelled collectively, a  
334 substantial proportion of the loading variation observed can be explained as a result of the  
335 biometric variation observed in tool users (up to 51%). The two traits remaining in the final  
336 model were Grip Strength and Pad-to-Side Pinch Strength, which were inseparable in terms of  
337 their contribution to the prediction in loading levels, with 49% of the normal force variation  
338 explained by these two attributes. First-to-second digit ratio was the third strongest predictive  
339 variable, followed by the lengths of digits one through three. Tip-to-tip Pinch Strength and  
340 Hand Length were the first two attributes removed from the model. It is important to note that  
341 early removal from this model does not mean that traits do not have a significant impact on  
342 handaxe loading levels, just that they make a weaker contribution to the prediction of handaxe  
343 loading levels relative to traits in later models.

344 The 13 tool-form attributes, when entered into a BSR, resulted in 13 model steps  
345 (Supplementary Table 2). Edge angle was the only predictive variable to remain in the final  
346 model.  $R^2$  values were substantially reduced relative to the biometric variables, with tool-form

347 attributes explaining <6% of the loading variation in all models. Position of Maximum Width,  
348 Shape, and Elongation were the second, third and fourth strongest predictive variables,  
349 although it should again be stressed that they made a relatively low contribution. In sum,  
350 although an order of contribution has been produced, with Edge Angle making the greatest  
351 contribution towards the prediction of handaxe force capabilities, it appears the tool-form  
352 attributes examined here have a limited impact on handaxe loading.

353 Differences between the predictive power of biometric and tool-form traits are also  
354 highlighted by the individual linear regressions run with the three strongest predictors of  
355 handaxe loading for each type of trait (Table 4). The only tool-form attribute to significantly  
356 predict handaxe loading levels was again demonstrated to be Edge Angle, while all three  
357 biometric traits returned statistically significant values. There was also a marked difference in  
358 the strength of  $R^2$  values in the two types of variable (Table 4). Indeed, between 20–48% of  
359 loading variation can be explained by the three biometric traits, while <3% of applied force can  
360 be explained by tool-form attributes.

#### 361 **4. Discussion**

362 Variation in tool-user biometric traits and tool-form attributes have both been demonstrated to  
363 influence the functional performance of stone tools (Walker, 1978; Jobson, 1986; Prasciunas,  
364 2007; Collins, 2008; Key and Lycett, 2018; Clarkson et al., 2015). ‘Loading’ is a crucial  
365 variable in the performance of a cutting tool (Atkins, 2009; Key 2016), being directly related  
366 to the generation of ‘cutting stress’ (force per unit area). Presented here are data investigating  
367 the comparative influence that biometric variables and tool-form variables have on the loading  
368 capabilities of Acheulean handaxes. Although handaxe effectiveness has long been a point of  
369 interest in experimental archaeology studies (e.g., Leakey, 1950; Jones, 1981; Machin et al.,  
370 2007; Shea, 2007; Toth and Schick 2009; Galán and Domínguez-Rodrigo, 2014), loading has  
371 not previously been examined in these tools. Our data reveal that tool-user biometric variation  
372 can have a substantially greater impact on loading relative to tool-form attributes. This  
373 difference is demonstrated here by up to a factor of up to ten.

374 Collectively, these results highlight that not all variables relevant to the efficient and  
375 effective use of stone tools are equally influential. In turn, we contend that when considering  
376 how effectively Palaeolithic hominins were able to use handaxes, an individual’s ability to  
377 forcefully secure, grip and manipulate these tools was by far the most important factor, relative  
378 to the morphology of the tool being used. Effective handaxe use was, therefore, influenced to

379 a greater extent by the biometric condition and biomechanical capabilities of the hominin using  
380 the tool, relative to the form of the tool itself.

381 The disparity observed here is particularly surprising given the coefficient of variation  
382 levels present in each category of variable. Ordinarily, in terms of prediction, it would be  
383 expected that the independent variable(s) exhibiting the greatest levels of variation would show  
384 higher levels of correlation with the dependent variable. As revealed in Tables 1 and 2,  
385 however, the variation observed in the tool-form attributes is, in most instances, greater than  
386 those seen in the biometric traits. Despite the greater variation in many of the tool-form  
387 attributes, it is the biometric traits, with their relatively lower CV levels, that have greater  
388 impact on loading. These data, therefore, further underline the importance of a tool user's  
389 biometric condition when considering stone-tool functional performance.

390 Our data support previous research emphasising areas of functionally related 'free play' in  
391 handaxe morphology, where variation in form has a potentially limited impact on performance  
392 (Isaac, 1972; Crompton and Gowlett, 1993: 177; Lycett et al., 2016). Indeed, previous research  
393 has indicated that shape, size, and symmetry (Machin et al., 2007; Key and Lycett, 2017b) have  
394 only limited impact on a handaxe's ability to be used as a cutting tool; at least until  
395 morphological 'thresholds' are reached (Key and Lycett, 2017b). As experimentally confirmed  
396 elsewhere, however, some specific tool form attributes do have significant influences on stone  
397 tool performance (e.g., Clarkson et al., 2015; Key et al., 2018). Further, we acknowledge that  
398 the present analyses are absent of the dynamic motions required during cutting actions, with  
399 some variables potentially being of greater relevance during such motions (e.g., Simão, 2002;  
400 Gowlett, 2006). This includes the length and uniformity of a handaxe's cutting edge, where the  
401 sweeping motion used in some cutting actions could have a greater impact than observed here  
402 where the focus is on loading. Moreover, a few handaxes at the upper extremes of the size  
403 variation, while serviceable in a downward plane, may become unwieldy with one hand when  
404 used in more complex motions. Nonetheless, a stone tool's loading potential is a relevant and  
405 important factor in determining its functional performance, and investigation of the variables  
406 influencing this metric is vital to understanding the capabilities of stone tools in prehistory.  
407 Our data suggest, therefore, that the selective pressures on handaxe form relating to loading  
408 potential would be relatively low, allowing for substantial variation in the range of tool  
409 morphologies produced by Acheulean hominins. The considerable variation observed in  
410 archaeological handaxe forms across different sites (e.g., Wynn and Tierson 1990; Chauhan  
411 2010; Gowlett, 2013; Norton et al., 2006; Petraglia and Shipton, 2009; Lycett and von Cramon-

412 Taubadel, 2015), and even within individual sites (e.g., Crompton and Gowlett, 1993; Gowlett,  
413 2006, 2013; Archer and Braun, 2010; Wang et al., 2014; Moncel et al., 2016), also supports  
414 the notion that hominins likely had a relatively large degree of freedom when producing  
415 functionally viable bifaces (at least for a majority of traits).

416 Our finding that edge angle significantly influences handaxe loading levels is consistent  
417 with previous research detailing its impact on biface cutting performance. As demonstrated by  
418 Key et al. (2016), the relationship between handaxe edge angle variation and cutting  
419 performance is complex and depends on both the ease of cutting stress creation between the  
420 tool and worked materials, and the tool user's ability to exert high working loads through the  
421 tool. Our data speak to the latter side of that equation, and indicate that more obtuse edges on  
422 handaxes facilitate the exertion of greater loading levels by tool users' hands onto the tool. This  
423 additional force is then transferred through the tool and onto the worked material. Indeed, the  
424 more obtuse the edge, the greater the tool's surface area in contact with the hand, and the lower  
425 the stress exerted by the tool on the skin (therefore reducing the risk of injury and pain).  
426 Previous suggestions (e.g., Gowlett 2006; Grosman et al., 2011; Key et al., 2016) that  
427 Acheulean hominins intentionally produced the more obtuse base ('butt') edges observed on  
428 handaxes in response to ergonomic considerations are, therefore, strengthened by the present  
429 data.

430 Our data also reaffirm the significant and strong impact that biometric variation in a tool-  
431 user's hands can have on the functional performance of stone tools. Previous works by Rolian  
432 et al. (2011) and Key and Lycett (2018) have demonstrated how variation in the size, strength,  
433 and digit ratios of an individual's hands have potential to influence how effectively Lower  
434 Palaeolithic stone tools can be used, and the subsequent impact on cutting performance. Here,  
435 we demonstrate that loading potential, a previously under-investigated performance  
436 characteristic, is also significantly and strongly influenced by biometric variation in the hand.  
437 Most notably, individuals with increased precision-grip strength capabilities can apply  
438 significantly greater force through handaxes during their use. For hominin populations where  
439 stone tool use was important to their survival, it is therefore reasonable to hypothesize that  
440 those individuals able to more capably apply stone tools could have had a selective advantage,  
441 and the phenotype underpinning this capability would have been passed to successive  
442 generations.

443 It is important to acknowledge that the present results were generated from a sample of  
444 individuals displaying modern human (*Homo sapiens*) hand anatomy and corresponding levels  
445 of biometric variation. Given that the precision-gripping capabilities of *H. sapiens* are  
446 hypothesized to have been selectively favoured over millions of years (Tocheri et al., 2008;  
447 Marzke, 2013; Kivell, 2015), it is arguably the case that the participant sample used here  
448 displays lower levels of variation than that observed in early tool using populations; potentially  
449 indicating the observed relationships to have been stronger during the Lower Palaeolithic.  
450 Differences in hand anatomy between modern humans and Lower Palaeolithic hominin species  
451 do, however, raise questions about how accurately results can be applied to prehistoric  
452 populations. Fossil hand remains from the earliest hypothesized tool-using hominin species (>  
453 2 Mya) often indicate a transitional anatomy, with some human-like precision manipulative  
454 capabilities (Tocheri et al., 2008; Kivell, 2015). While hand remains from between ~1.8–0.3  
455 Mya are rare, those available indicate additional modern human-like features (Dominguez-  
456 Rodrigo et al., 2015; Lorenzo et al., 2015), such as the styloid process on the third metacarpal  
457 (Ward et al., 2014). Hence, while it is not yet precisely clear how different modern human and  
458 Acheulean hominin hand anatomy is, we would argue based on these known similarities, that  
459 the relationships observed here can also be attributed to Acheulean species. Irrespective of the  
460 hand anatomy of handaxe using hominins, however, there would have been variation on the  
461 population level, against which selective pressures could have acted.

462 Finally, the loading ranges recorded here are substantial, with up to ~24 kgf being exerted  
463 through a handaxe. Although such high values were rare, with only seven individuals recording  
464 mean forces of 10 kgf or above for at least one of their utilized tools, it is arguably the case that  
465 the modern, relatively sedentary, lives of the participants restricted the number of individuals  
466 able to exert higher loads. While these forces are unlikely to be applied during typical ‘slice  
467 push’ cutting motions (Atkins et al., 2004; Atkins, 2009), as observed when slicing through  
468 animal flesh, for example, it is nonetheless clear that substantial forces can be applied through  
469 a handaxe’s working edge. Other cutting activities that more heavily depend on load  
470 application in single plane, such as forcing apart joint sockets or digging tubers from the  
471 ground, may profit from the exertion of particularly high loads. This would indicate that ruling  
472 out hypothesized functions for handaxes based solely on their requirement for high working  
473 loads is not necessarily justified.

## 474 **5. Conclusion**



475           Here, we demonstrate that biometric attributes, most notably an individual's precision-  
476 grip strength, more readily predict handaxe loading levels relative to tool-form variables.  
477 Indeed, up to ~50% of the force applied through the cutting edge of a handaxe can be attributed  
478 to the biometric condition of the individual using that tool. Multiple regression of 13 tool-form  
479 attributes could only account for ~5% of a handaxe's loading potential. Predictive models of  
480 Acheulean handaxe functionality should, therefore, take greater account of the anatomy and  
481 manipulative capabilities of the individual using the tool, relative to the form of the tool being  
482 used. Moreover, the selective pressures acting on both hominin anatomy and stone-tool  
483 morphology were likely to have been disparate during the Palaeolithic. Overall, these results  
484 help explain the derived, precision-and-manipulation focused hand anatomy observed in *H.*  
485 *sapiens*. They also, however, underline why archaeological handaxe forms may have been free  
486 to vary in form across time and space without necessarily incurring critical impacts on their  
487 functional capabilities.

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